



Design and Simulation of Control Circuit for Single Phase Cycloconverter

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ABSTRACT: The most commonly used motors in recent days are induction motors due to its simple construction and less expensive compared to DC motors. But the main drawback of induction motor compared to separately excited DC motor is that it is a constant speed motor. Hence in the past, induction motors have been used primarily in constant speed applications. Variable frequency is essential in most of the industrial applications and the recent advancement in the power electronics field makes this task easy by using the power semiconductor devices. There are many techniques used to vary the supply frequency, out of which cycloconverter is one of the commonly used techniques. Among all the methods this is simple, reliable and economical. The objective of the paper is to design a control circuit to provide a proper sequence of pulses for the semiconductor switches of the cycloconverter power circuit. The control circuit is designed using the Op amps and logic gates. The designed control circuit is simulated using the OrCAD Pspice software.

KEYWORDS: Astable multivibrator; Cycloconverter; Control circuit; Frequency; Monostable multivibrator

I. INTRODUCTION

The Cycloconverter is basically ac to ac power converters where the alternating voltage at supply frequency is converted directly to a lower frequency without going through any intermediate dc power conversion stage [1]. The variable frequency has always been of great importance in the industrial applications. This is because some electrical devices need variable frequency ranging from one tenth to one third of the supply frequency. Cycloconverter helps in achieving this variable frequency. The Cycloconverter has been traditionally used only in very high power drives, usually above one megawatt. Some examples are tube mill drives above 5MW [2], Ship propulsion drives [3], induction motors used in AC traction, aircraft power supplies etc [4]. The power rating of Cycloconverter ranges from few megawatts up to many tens of megawatts and hence they are usually constructed using naturally commutated thyristors. The Cycloconverters are generally used for speed control of induction motor and synchronous motor below the rated speed. Analysis of induction motors controlled with Cycloconverter has been investigated extensively over recent years.

II. RELATED WORK

In [4] a single phase cycloconverter circuit which could generate variable frequency is designed. The proper generation of the blanking and gate pulses of the switching devices and synchronizing them with the input signal is the most important thing in designing a cycloconverter circuit which becomes easier due to the availability of the integrated circuit. Here 555 timer and operational amplifier IC's have been used for generation of blanking and triggering signals. The synchronization of these signals with the input signal is performed by means of the comparator circuit where the operational amplifier IC is used. Due to the cost constraint, a transformer of secondary rating of 9V and 800mA is considered for designing the cycloconverter which delivers a power of about 7W. [6] proposes an analysis of the interharmonics currents behavior under an unbalanced load, injected by a cycloconverters with 12-pulse configuration and multi-winding transformers. Three-phase transformers with two secondary windings with star and delta connection and a three-phase RL load with a decoupled direct current load control are used to simulate the system.

International Journal of Innovative Research in Computer and Communication Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 7, July 2015

[7] Evaluates three different modelling options for the SAG mill drive. The first option considers a complete model in phase and $qd0$ variables of the two-stator-winding synchronous motor fed by two six-pulse cycloconverters. The second option develops a winding rotation transformation to obtain an equivalent one-stator-winding synchronous motor, which is fed by a 12-pulse cycloconverter. The third model considers the equivalent one-stator synchronous motor fed by an ideal converter that produces purely sinusoidal voltage and current waveforms. Each model is evaluated during steady state, step speed commands, and step load disturbances.[8] This paper describes the characteristics of low frequency ac transmission system using cycloconverters with three configurations. New control scheme is also provided for all operating transmission system. Cable and filter selection are also included in this paper.

[9] A De-Re-coupling uni-polarity phase-shifted control strategy is proposed. The waveform control method can achieve zero voltage switching (ZVS) of all the switches in the matrix/cycloconverter and natural commutation of the filter inductance without auxiliary circuits and commutation overlap of the matrix/cycloconverter. [10] Cycloconverter control circuitry is discussed using examples from a practical three-phase to single-phase circulating current free cycloconverter. The voltage biased cosine wave technique is used for phase control. [11] This paper presents a new control method for three-phase to single-phase cycloconverters based on pulse width modulation (PWM) technique. Due to the proposed control method, the desired output voltage can be generated even with unbalanced input voltages. The proposed control method can easily be extended to three-phase to n -phase cycloconverters.

III. SINGLE PHASE CYCLOCONVERTER

The power circuit of Single phase Cycloconverter mainly consist of two converters, positive and negative converters. The positive converters are used to get the positive half cycle of output voltage and the negative converters are used to get negative half cycle of output voltage. The control circuit should provide a correct sequence of pulses for the operation of two converters [12]. The transformer is used for providing alternating output to the load. The power circuit of single phase cycloconverter is shown in Fig. 1 and the input and output voltage waveform is shown in Fig. 2.

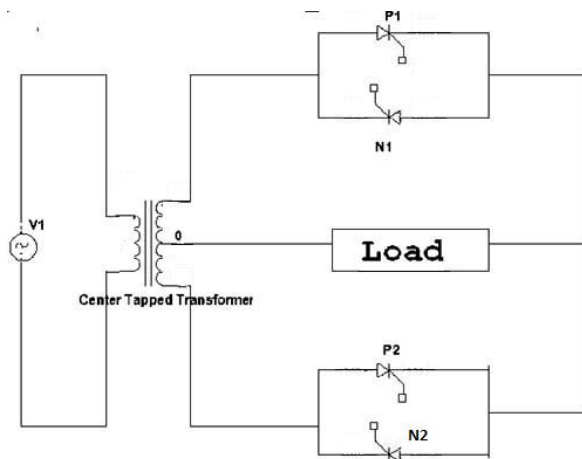


Fig.1. The Power Circuit of Single phase Cycloconverter

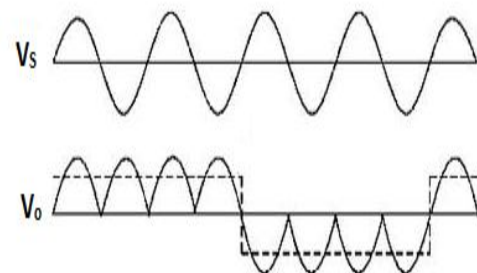


Fig. 2. Input and Output voltage waveform

A Cycloconverter circuit is comprised of power, control and filter sections. The power section of Cycloconverter comprises of a dual converter in which two groups of controlled rectifiers (thyristors) employ a common centre tapped transformer as their source [5]. The main function of the control circuit is to produce trigger pulses in a particular sequence and feed them to the gates of the positive and negative group of thyristors so as to generate a voltage of desired wave shape at the output terminals of a cycloconverter.

International Journal of Innovative Research in Computer and Communication Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 7, July 2015

IV. DESIGN OF CONTROL CIRCUIT

There are two groups of converters which can be defined as P and N. The P and N converters control the positive and negative half cycles of the output voltage of the desired frequency respectively. The control circuit should be designed in such a way that the P converter goes in conduction during the positive half cycle of the input signal when the Q converter remains idle. Similarly when the Q converter goes in conduction during negative half cycle of the input signal the P converter remains idle. Two blanking signals P and N determine the operation of the thyristors in each converter group according to the sequence of the gate trigger. Moreover the frequency of the output signal depends on the frequency of the P and N blanking signals [13]. The functional block diagram proposed is shown in Fig.3

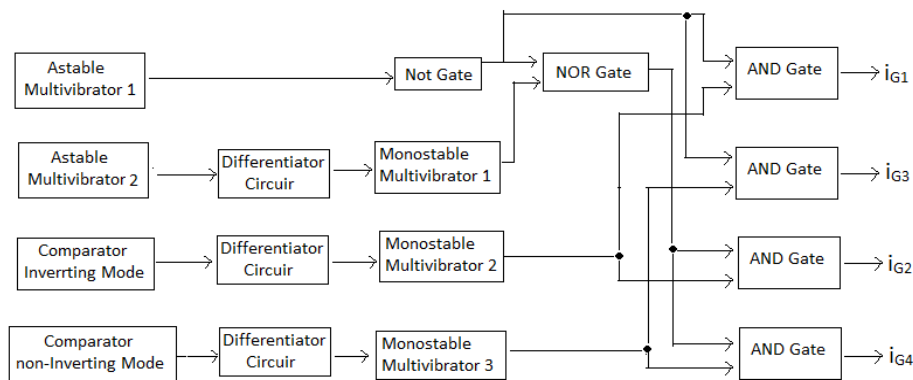


Fig.3. Functional Block diagram of the proposed method

Design Considerations

A. Astable Multivibrator:

Here Astable multivibrator 1 is designed to generate a square wave of frequency equal to the frequency of output voltage and Astable multivibrator 2 is used to generate square wave of frequency twice that of output voltage. This is constructed using transistors. The on time of the square wave is slightly less than the off time.

Let us consider the output frequency which should be reduced to 12.5 Hz i.e. one fourth of 50 Hz. The time period of square wave generated by Astable multivibrator 1 should be equal to 80 msec i.e. 12.5 Hz. Let the ON time be 39.6 msec and OFF time be 40.4 msec. Square wave of higher ON time is produced and it is inverted using NOT gate. This signal is P blank signal. Therefore, $T_1=40.4$ msec $T_2=39.6$ msec, Let $C_1=C_2=1\mu F$

$$T_1=0.693R_1C_1 \quad \text{eq. (1)}$$

$$T_2=0.693R_2C_2 \quad \text{eq. (2)}$$

Solving eq. (1) and eq. (2) we get,
 $R_1=58297\Omega$ and $R_2=57143\Omega$

The N blank signal which is phase shifted by 180° with P blank signal is generated using Astable multivibrator 2. The output frequency of Astable multivibrator 2 should be twice that of frequency of Astable multivibrator 1 i.e. 25 Hz. The time period is 40 msec, let $T_1=27$ msec $T_2=13$ msec. Let $C_1=C_2=1\mu F$

$$T_1=0.693R_1C_1 \quad \text{eq. (3)}$$

$$T_2=0.693R_2C_2 \quad \text{eq. (4)}$$

Solving eq. (3) and eq. (4) we get,
 $R_1=38961\Omega$ and $R_2=18760\Omega$

International Journal of Innovative Research in Computer and Communication Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 7, July 2015

The output of Astable multivibrator 2 is passed through differentiator circuit to get a spike. This spike is used to trigger an Monostable multivibrator. The output of monostable multivibrator is NORed with P blank signal to get N blank signal. For synchronization between the blanking signals P and N it is required to set the charging of the capacitors of both astable multivibrators at the same instant. The basic Astable multivibrator circuit using transistors is shown in Fig.4

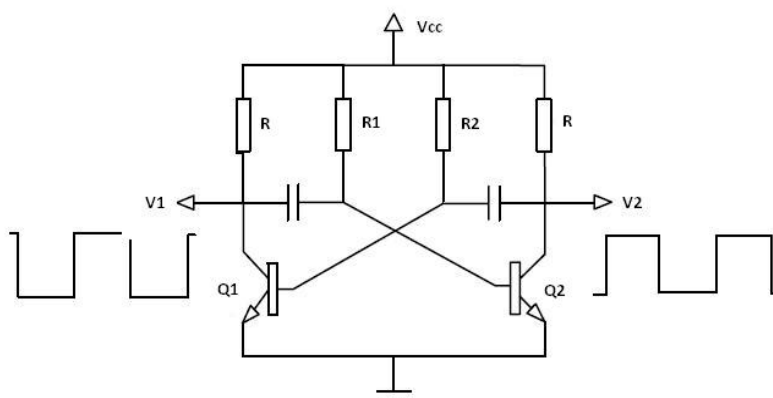


Fig.4. Astable multivibrator using transistors

B. Differentiator Circuit:

The thyristor should be triggered by the pulses which have the duration just greater than on time therefore the gate triggering of the thyristor by the above generated pulses is unfeasible. If the above square waveforms are used for gate triggering of the thyristor then huge power dissipation can be destructive for the thyristor and the negative pulses cause the thyristor to the false triggering. This difficulty can be eliminated by using the differentiator circuit which gives narrow spikes for thyristor gate triggering. The differentiator circuit and its output are shown in the Fig.5.

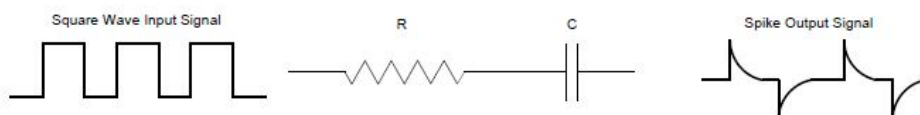


Fig.5. Differentiator circuit and its output

C. Monostable Multivibrator:

The spikes generated from differentiator circuit is used to trigger Monostable multivibrator. The circuit diagram of monostable multivibrator using transistor is shown in Fig.6. By adjusting the RC time constant of the multivibrator it is possible to obtain the output pulse (only positive) of any time period with the frequency half of the triggering spikes. The output pulse of the Monostable multivibrator is the trigger pulse, therefore the time period of the output pulse should be longer than the turn on time of the selected thyristor. Generally the turn on time of the thyristor is within the range of 150 to 200 μ sec. In this case the RC time constant is considered of 220 μ sec by selecting $C = .022\mu$ f, $R = 10k\Omega$, $R_f = 10k\Omega$ and $RC=1k\Omega$ and $V_{cc}=15v$. So by using the combination of the differentiator circuit and the monostable multivibrator, the positive pulse of the duration 220 μ sec is obtained. These pulses are properly synchronized with the input signal.

International Journal of Innovative Research in Computer and Communication Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 7, July 2015

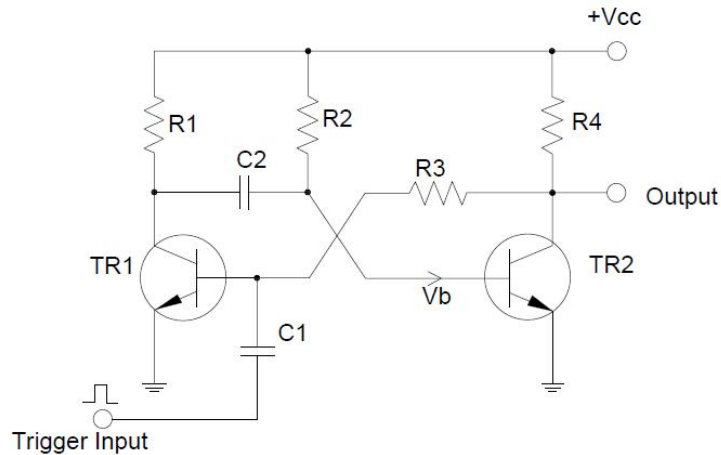


Fig.6. Monostable multivibrator using transistor circuit

D. Synchronizing signal generation:

Two comparators are used in both inverting and non inverting mode and the outputs of them are fed to the differentiator circuit to get the Synchronizing signal. The parameters of the differentiator circuits are $R = 10\text{k}\Omega$, $C = 0.01\mu\text{F}$ and the RC time constant is $100\mu\text{sec}$. The differentiated signals of the differentiators are fed into the Monostable multivibrator and the parameters of the Monostable multivibrator are $R = 10\text{k}\Omega$, $C = 0.22\mu\text{F}$, $R_C = 1\text{k}\Omega$ and $R_f = 10\text{k}\Omega$. This generates train of pulses with time period of $220\mu\text{sec}$ in both inverted and non-inverted mode. Finally the triggering pulses for thyristors are generated using the combinations of the AND gates as shown in the Fig. 3.

The expected pulse sequence output to get one fourth of the supply frequency is shown in Fig. 7.

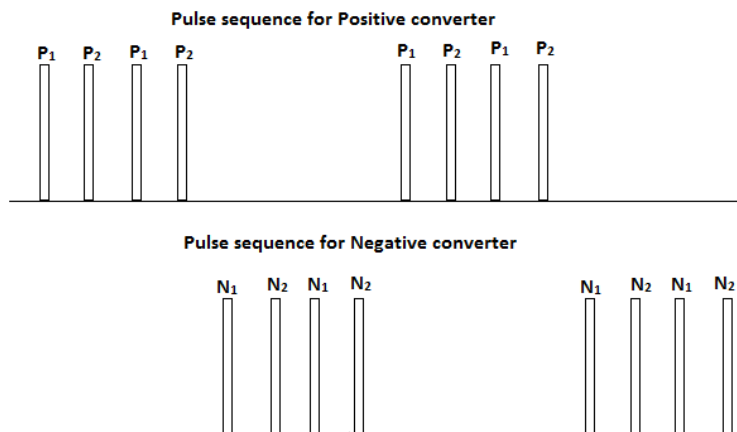


Fig.7. Expected Pulse Sequence of control circuit

V. SIMULATION AND RESULTS

The proposed method is simulated using ORCAD Pspice, version 10.3 software. The Detailed Circuit Diagram of control circuit of single phase Cycloconverter is shown in Fig. 8. Using Astable multivibrator 1, the on time of the square wave is generated slightly less than the off time which is inverted using NOT gate as discussed earlier in section IV. This signal is P blank signal. The N blank signal which is phase shifted by 180° with P blank signal is generated using Astable multivibrator 2.

International Journal of Innovative Research in Computer and Communication Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 3, Issue 7, July 2015

The resistance values of R_1 and R_2 of Astable Multivibrator 1 and 2 using eq. (1) to eq. (4) for various frequencies is tabulated as shown in Table 1. The narrow spikes for thyristor gate triggering obtained from differentiator circuit is fed to Monostable multivibrator circuit and the time period of the output pulse longer than the turn on time of the selected thyristor is obtained. The circuit is designed and the synchronizing signal in inverting and non-inverting mode using comparators and AND gate combination is obtained to get the expected pulse sequence as shown in the Fig. 7. The ON time of the generated pulse was designed for $220\mu\text{sec}$. The simulated pulse sequence obtained is shown in Fig. 9. The result shows pulse sequence for positive and negative converter. Here the top half of the simulation shows red pulse indicating positive converter thyristor P1 and green pulse indicating negative converter thyristor P2. Similarly the lower half of the simulation shows green pulse indicating positive converter thyristor N1 and red pulse indicating negative converter thyristor N2. The simulation result obtained matches the expected result.

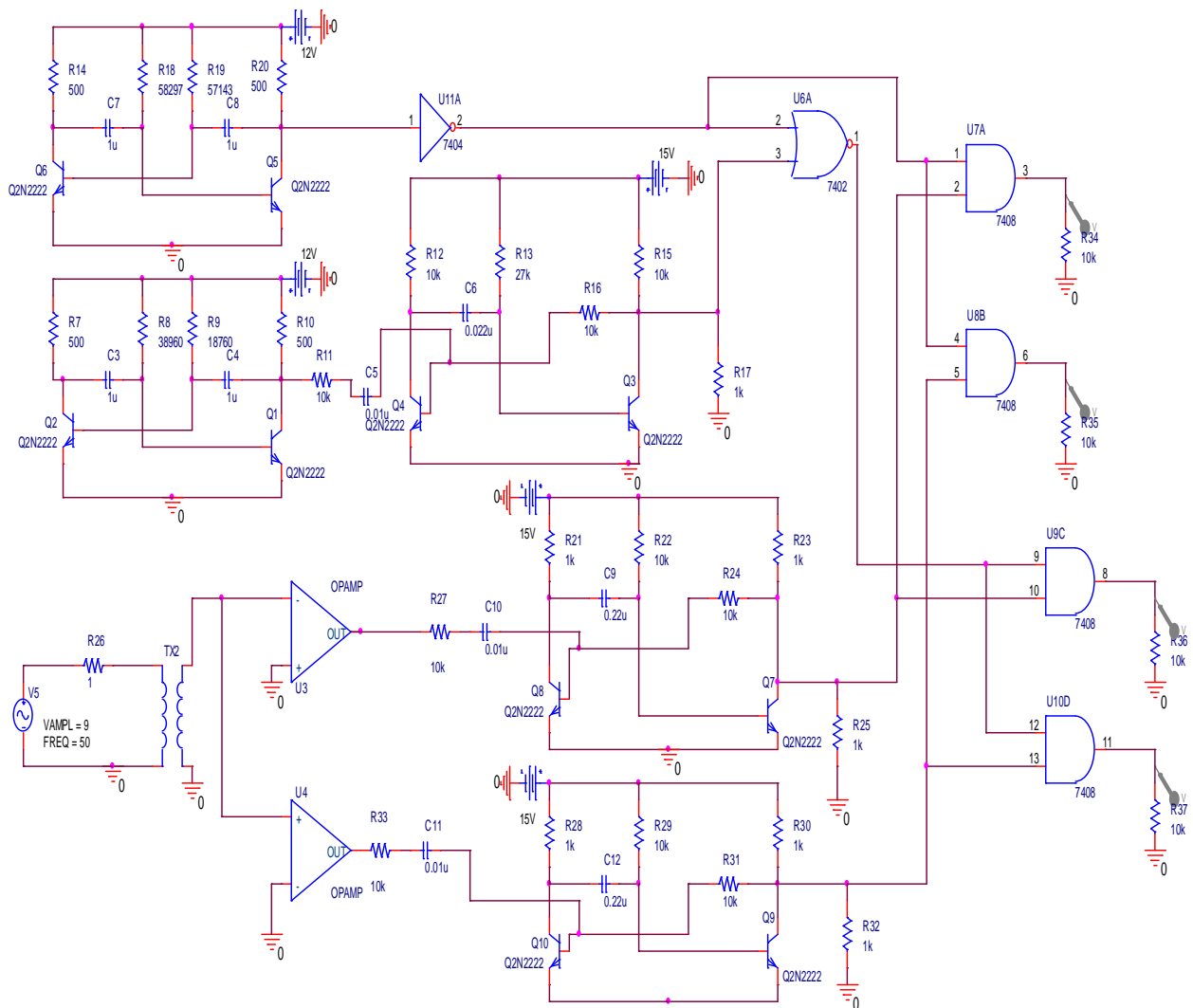


Fig.8. The Detailed Circuit Diagram of Cycloconverter

International Journal of Innovative Research in Computer and Communication Engineering

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Vol. 3, Issue 7, July 2015

| Supply Frequency (f) f=50 Hz | Astable Multivibrator 1 | | Astable Multivibrator 2 | |
|---------------------------------|-------------------------|--------------------|-------------------------|--------------------|
| | R ₁ (Ω) | R ₂ (Ω) | R ₁ (Ω) | R ₂ (Ω) |
| f/2 | 29437 | 28283 | 19480 | 9380 |
| f/3 | 43867 | 42713 | 29220 | 14069 |
| f/4 | 58297 | 57143 | 38961 | 18760 |
| f/5 | 72727 | 71572 | 48629 | 23376 |

Table 1. Resistance values of Astable multivibrator 1 and 2 for various frequencies

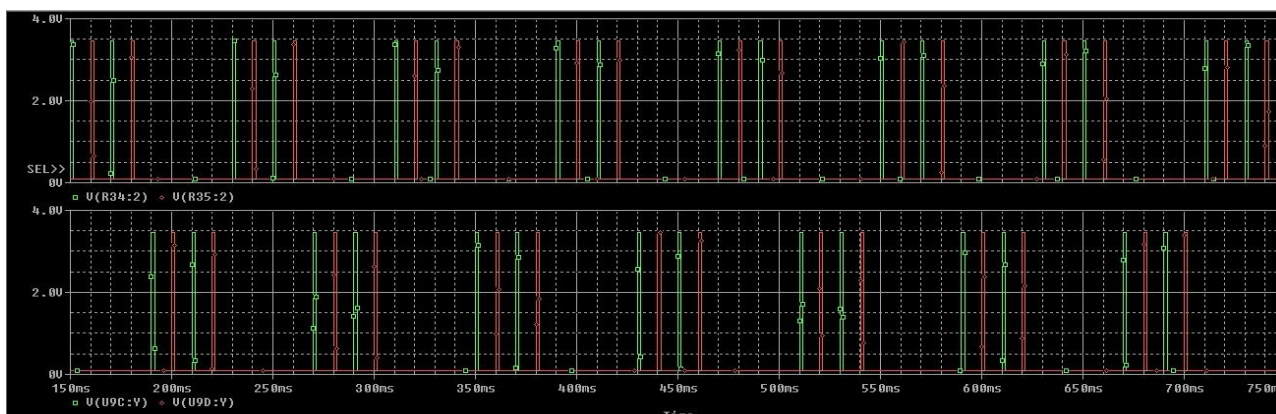


Fig.9. Simulated Output of Control Circuit of Cycloconverter

VI. CONCLUSION

As stated earlier many of the industrial applications requires variable frequency. The cycloconverter plays a pivotal role in achieving this task. This control circuit designed and simulated using Op amps and logic gated achieves the expected results. Further this technique can be extended for three phase cycloconverter. By achieving the variable frequency, in many applications the DC motors can be replaced by Induction motor.

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